

QASIM BNR BOYUTLANDIRMA YÖNTEMİ

Ref: QASIM '99, page 475, 13-11 Design Example

GİRİŞ

Qasim (Wastewater Treatment Plants, 1999) da verilen BNR boyutlandırma yöntemi karbon giderimi nitrifikasyon ve denitrifikasyon için kullanılabilir θ_{CA} , θ_{CDN} , $Y_{obsBOD5}$, Y_{obsN} , Y_{obsDN} değerlerinin Kinetik parametreler kullanılarak hesaplanmasına dayanır. Bu değerler bilindiği takdirde karbon gidermesi, nitrifikasyon ve denitrifikasyon, bakteri üretim hızları: (P_{XBOD5} , P_{XN} , P_{XDN})

$$P_{XBOD5} = QY_{obsBOD5}(S_0 - S)$$

denklemleri kullanılarak ve gerekli, oksik ve anoksik hacimler ise;

$$\theta_c = \frac{VX}{P_x}$$

denklemlerini kullanarak hesaplanır. Bu metotta Lawrence & McCarthy metodunda olduğu gibi, deneme ve yanılma metodu kullanılmaz.

BESİ KÜTLE KORUNUMU (NUTRIENT MASS BALANCES)

1. Nitrojen Kütle Korunumu

$$\text{TN to be Nitrified} = \text{TN to N} = \text{TKN}_{in} - \text{TKN}_{eff} - \text{OrgN} - \text{assim}$$

$$\text{OrgN} - \underbrace{\text{assim}} = 0.122 Y_{obsBOD5}(S_0 - S)$$

g OrgN/g VSS

Hücrenin %12.2'si azot kabul edilir (12.2 % of the microbial cell $C_{60}H_{87}O_{23}N_{12}P$ is assumed to be N.)

$$\text{NO}_3\text{N to DN} = \text{TN to N-} (\text{NO}_3\text{N}_{\text{eff}})$$

2. Karbon Kütle Korunumu

$$\text{BOD}_5 \text{ to be satisfied} = (S_0 - S) - \left(\text{BOD}_5 \text{ consumed due to DN} \right) - \left(\text{BOD}_5 \text{ consumed due to deoxygenation} \right)$$

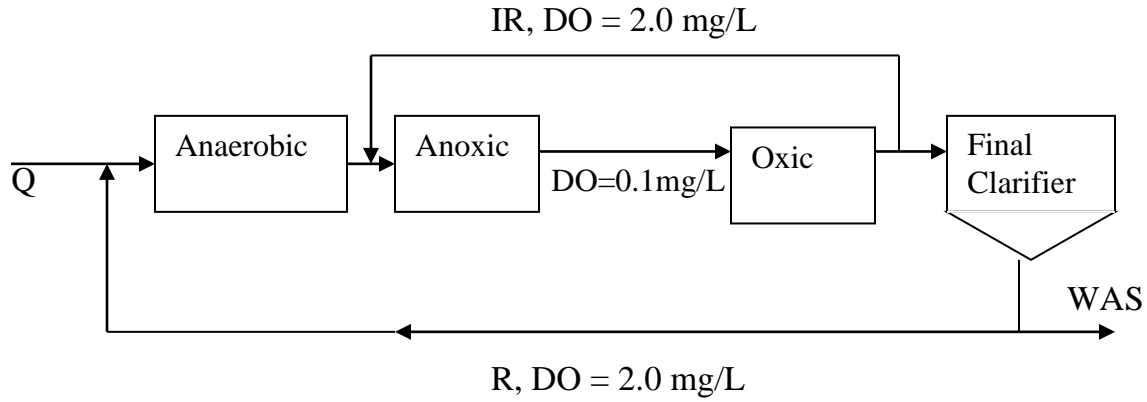
$$\left(\text{BOD}_5 \text{ consumed due to DN} \right) = (0.68)(3.7)(\text{NO}_3\text{-N to be DN}) \frac{g\text{BOD}_L}{g\text{NO}_3 - \text{N}}$$

Artık çözülmüş oksijen giderilmesi için gerekli BOD₅ miktarı (BOD₅ consumed due to Deoxygenation) az olduğu halde kütle korunumuna ilave edilecektir.

$$\left(\text{BOD}_5 \text{ consumed due to deoxygenation} \right) = (0.68) \underbrace{(1.3)}_{g\text{BOD}_L/g\text{DO in return flow}} [(\text{IR}+\text{R})\text{DO}_{\text{maxN}} - (1+\text{IR}+\text{R})\text{DO}_{\text{maxDN}}]$$

$$\text{DO}_{\text{maxDN}} = 0.1 \text{ mg/L}$$

$$\text{DO}_{\text{maxN}} = 2.0 \text{ mg/L}$$



HETEROTROF VE OTOTROFLARIN ÜREME HIZLARI (Production (P) of Heterotrophs and Autotrophs)

$$\theta_{cA} = \frac{SF_{kinetic} SF_{process}}{\mu'_{max A} - k_{dA}}$$

$$\mu'_{max A} = \mu_m e^{0.098(t-15)} \frac{DO}{DO + K_{DO}} [1 - 0.833(7.2 - pH)]$$

$SF_{kinetic} = 2.0$ $\mu_m = 0.47$ (0.3 – 3.0d⁻¹) DO = 2.0 mg/L
 $SF_{process} = 1.5$ $K_{DO} = 1.0$ (1.0 – 1.3 mgDO/L)

$$Y_{obs N} = \frac{Y_N}{1 + k_{dN}(\theta_{cA})}$$

$Y_N = \text{Range } 0.1 - 0.3, \text{ Typical } 0.2$
 $k_{dN} = 0.05d^{-1} (0.03-0.06d^{-1})$

$$Y_{obs BOD_5} = \frac{Y_{BOD_5}}{1 + k_{dBOD_5}(\theta_{cA})}$$

$$\frac{1}{\theta_{c,A}} = \frac{\mu'_{\max A} (NH_4 - N)_e}{K_N + (NH_4 - N)_e}$$

$$K_N = 10^{0.051t - 1.158}$$

$P_{X_N} = Y_{\text{obs}_N} Q$ (TN to be DN) \rightarrow kg/day, Production rate of Autotrophs (Nitrifiers)

$P_{X_{\text{BOD}_5}} = Y_{\text{obs}_{\text{BOD}_5}} Q$ (BOD₅ to be Satisfied) \rightarrow kg/day, Production rate of carbonaceous bacteria

$$\theta_{c, \text{DN}} = \frac{SF_{\text{DN}}}{\mu_{\max \text{DN}} \theta_{\text{DN}}^{t-20} (1 - DO_{\max \text{DN}}) - k_{\text{dDN}}}$$

$$SF_{\text{DN}} = 1.5$$

$$\mu_{\max \text{DN}} = \text{Range} - 0.2-0.4, \text{ Typical} = 0.3$$

$$\theta_{\text{DN}} = \text{Range} - 1.03-1.20, \text{ Typical} = 1.03$$

$$DO_{\max \text{DN}} = 0.1 \text{ mg/L}$$

$$k_{\text{dDN}} = \text{Range} 0.02-0.08, \text{ Typical} 0.04$$

$$Y_{\text{obs}_{\text{DN}}} = \frac{Y_{\text{DN}}}{1 + k_{\text{dDN}}(\theta_{c, \text{DN}})}$$

$$Y_{\text{DN}} = \text{Range} 0.5 - 0.7, \text{ Typical} 0.6$$

$$P_{X_{DN}} = Y_{obsDN} Q \text{ (NO}_3\text{-N to be DN)}$$

→ kg/day, Production rate of denitrifiers

$$P_{XH} = P_{X_{BOD5}} + P_{X_{DN}}$$

Heterotrophic

→ kg/day, (Production rate of heterotrophs)
Heterotrof üreme hızı

$$P_{XA} = P_{X_N}$$

Autotrophic

→ kg/day, (Production rate of autotrophs) Ototrof üreme hızı

Sonuç (Result):

$$\text{Increase in MLVSS} = P_{X_T} = P_{X_{BOD5}} + P_{X_{DN}} + P_{X_A}$$

$$WAS = P_{X_T} / f_{VSS}$$

$$f_{VSS} = \frac{MLVSS}{MLSS}$$

REAKTÖR HACMİ HESAPLARI (REACTOR VOLUME CALCULATIONS)

Heterotrofların denitrifiye edilebilen yüzdesi = 50%

$f_{X_{DN}}$: Fraction of heterotrophs that can DN ≈ 0.5

$$f_{X_{DN}} = X_{DN} / X_H$$

$$V_{DN} = \frac{(\theta_{c, DN}) P_{X_{DN}}}{(f_{X_{DN}}) (X_{TVSS})}$$

$$f_{X_{DN}} = 0.5$$

$$V_{ABOD5} = \frac{(\theta_{c, A}) P_{X_{BOD5}}}{(f_{X_H}) (X_{TVSS})}$$

$$f_H = 0.94$$

